

Micah Swartz, P.E.	Project Number:	MS24-05004	
	Project Name:	F-4500 Swinging Door (OSW)	
	Date:	5/23/2024	Page:

**Product Approval Supporting Calculations
Alternative Anchorage Analysis & Design
R1 - Admin Update**

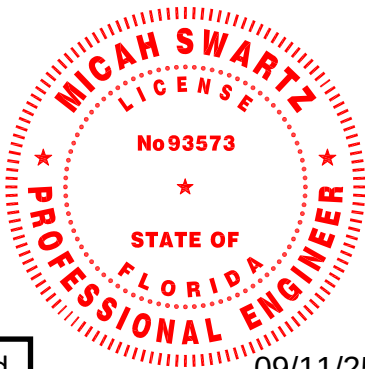
Project Number: MS24-05004

Drawing Number: D1000255

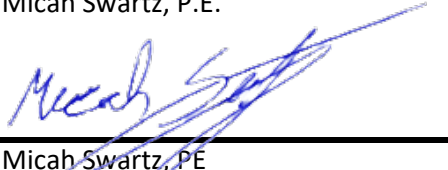
Reference Test Report: NCTL-310-23-019

Product Name: F-4500 Swinging Door (OSW)

Prepared for:
Jeld-Wen Windows & Doors
3737 Lakeport Blvd.
Klamath Falls, OR



Prepared by:
Micah Swartz, P.E.



Micah Swartz, PE
Florida License No. PE 93573

This item has been digitally signed and sealed by Micah Swartz, P.E. on the date adjacent to the seal.

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09/11/25

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Scope:

Micah Swartz, P.E. is contracted by Jeld-Wen Windows & Doors to evaluate alternative anchorage for the product: F-4500 Swinging Door (OSW). This evaluation is based on testing performed by National Certified Testing Laboratories (NCTL) in Everett, Washington, test report no.: NCTL-310-23-019 and dated 02/22/2023.

This evaluation does not include the air infiltration, water resistance or water penetration of the installation method or the installed product. In addition, the design of the building substrate to resist the superimposed loads is by others.

Reference Standards:

Current edition of the Florida Building Code, Building

ANSI/AWC NDS - National Design Specification (NDS) for Wood Construction

AISI S100 North American Specification for the Design of Cold-Formed Steel Structural Members

ICC-ES Report ESR-1976 ITW Buildex TEKS Self-Drilling Fasteners

ICC-ES Report ESR-2196 Hilti Self Drilling Screws to connect cold-formed steel

NOA 24-0102.06 Tapcon Concrete and Masonry Anchors with Advanced Threadform Technology

Certification of Independence:

In accordance with Rule 61G20-3 Florida Administrative Code, Micah Swartz, P.E. hereby certifies the following:

(1) Micah Swartz, P.E. does not have, nor does it intend to acquire or will it acquire, a financial interest in any company manufacturing or distributing products tested or labeled by the agency.

(2) Micah Swartz, P.E. is not owned, operated or controlled by any company manufacturing or distributing products it tests or labels.

(3) Micah Swartz, P.E. does not have, nor will acquire, a financial interest in any company manufacturing or distributing products for which the reports are being issued.

(4) Micah Swartz, P.E. does not have, nor will acquire, a financial interest in any other entity involved in the approval process of the product.

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Design Summary:

The table below summarizes the product: F-4500 Swinging Door (OSW) and their corresponding performance levels as established by testing.

Table 1: Summary of Test Results

Series/Model	Test Report Number	Size (W x H)	Performance
F-4500 Swinging Door (OSW)	NCTL-310-23-019 (02/22/23)	71.5 X 78.125	+ 50 psf / - 55 psf

As Tested Design:

Screw Information:

Screw Size: 8 Screw Embed: 1.5 in Edge Distance: 3/4 in (minimum)

Wood Screw Lateral: 106 lbs

Alternative Fasteners:

Screw Information:

Screw Size: 8 Screw Embed: 1.5 in Edge Distance: 3/4 in (minimum)

Wood Screw Lateral: 106 lbs

Tapcon Information:

Tapcon Size: 3/16 Embedment: 1-1/4 in (minimum) Edge Distance: 2-1/2 in (minimum)

Tapcon Lateral (Concrete): 155 lbs

Tapcon Lateral (CMU): 135 lbs

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Summary of Test Results - Plastics Checklist

Table 2: Summary of Test Results - Plastics Checklist

Product	Test Report Number	Test Standard	Performance
SMC Skin (fiberglass material)	ESP010982P	ASTM D638 (before and after G155)	-2.2% (averaged)
		ASTM D1929	770 °F (410 °C)
		ASTM D2843	62
		ASTM D635	Classification HB

The testing summarized in the table above was conducted by Element Materials Technology in St Paul, MN on 02/26/13 and meets the requirements listed in Miami-Dade County Checklist #0445, For the approval of: Plastic and Foam Plastic.

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Subject:
As Tested - Wood Screw Lateral Design - Single Shear

Input:

Calculation:

Screw Information:

Screw Size:
8

Screw Embed:
1.5
in

Root Diameter:
0.131
in

Main Member Type:
S-P-F
G:
0.42
F_{em}:
3,350
psi
thickness (t_m):
1.5
in

Side Member Type:
S-P-F
G:
0.42
F_{es}:
3,350
psi
thickness (t_s):
1.219
in

Lateral Design Factors - Table 12.3.1A (NDS)

D:	0.131	in	Diameter
F _{yb} :	100	ksi	Dowel Bending Yield Strength
F _{em} :	3,350	psi	Main Member dowel bearing strength
F _{es} :	3,350	psi	Side Member dowel bearing strength
l _m :	1.5	in	Main Member dowel bearing length
l _s :	1.219	in	Side Member dowel bearing length
R _d :	2.2		Reduction term - Table 12.3.1B (NDS)
R _e :	1		= F _{em} /F _{es}
R _t :	1.2		= l _m /l _s
k ₁ :	0.466		See Table
k ₂ :	1.111		See Table

Reference Lateral Design Values - Table 12.3.1A (NDS)

Z_{I_m}:
299
lbs

$Z_{Im} = \frac{Dl_mF_{em}}{R_d}$ (EQ 12.3 – 1)

Z_{II}:
113
lbs

$Z_{II} = \frac{k_1Dl_sF_{es}}{R_d}$ (EQ 12.3 – 3)

Z_{III_m}:
111
lbs

$Z_{III_m} = \frac{k_2Dl_mF_{em}}{(1 + 2R_e)R_d}$ (EQ 12.3 – 4)

Z_{IV}:
82
lbs

$Z_{IV} = \frac{D^2}{R_d} \sqrt{\frac{2F_{em}F_{yb}}{3(1 + R_e)}}$ (EQ 12.3 – 6)

Z_{MIN}:
82
lbs

Note: Side member is part of the Jeld-Wen assembly and verified during testing. Modes Z_{Is} and Z_{III_s} are not applicable to the calculation.

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Subject: As Tested - Wood Screw Lateral Design - Single Shear Cont.

Adjusted Lateral Design Values

$$Z' = Z * C_D * C_M * C_t * C_g * C_{\Delta} - \text{As per table 11.3.1 NDS}$$

C _D :	1.6	Load Duration Factor - Table 2.3.2 (NDS)
C _M :	1.0	Wet Service Factor - Table 11.3.3 (NDS)
C _t :	1.0	Temperature Factor - Table 11.3.4 (NDS)
C _g :	1.0	Group Action Factor - Section 11.3.6 (NDS)
C _Δ :	1.0	Geometry Factor - Section 12.5.1.1 (NDS)

$$Z': \quad 132 \text{ lbs}$$

Fastener Bending Across Shim Space

Ω:	1.67	
L:	0.25	in Maximum Shim Gap
D:	0.131	in Diameter
F _{yb} :	100	ksi Dowel Bending Yield Strength

$$\frac{F_{yb}}{\Omega} = \frac{M}{S} = \frac{16ZL}{\pi D^3} \Leftrightarrow Z = \frac{F_{yb} \pi D^3}{16 \Omega L} \qquad \text{Where } M = \frac{ZL}{2} \text{ (Guided Bending)}$$

$$Z_n/\Omega: \quad 106 \text{ lbs}$$

Bearing on Masonry Strap

Ω:	3.00	
F _u :	33	ksi Tensile Strength of strap
t:	20	GA
t:	0.036	in thickness of strap
D:	0.131	in

$$\frac{P_{nv}}{\Omega} = 2.7 * t * D * F_u - (EQ.J4.3.1 - 4, AISI S100)$$

$$P_{nv}/\Omega: \quad 140 \text{ lbs}$$

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Subject: Wood Screw Lateral Design - Single Shear

Input:

Calculation:

Screw Information:

Screw Size:

8

Root Diameter:

0.131

in

Screw Embed:

1.5

in

Main Member Type:

S-P-F

G:

0.42

F_{em}:

3,350

psi

thickness (t_m):

1.5

in

Side Member Type:

S-P-F

G:

0.42

F_{es}:

3,350

psi

thickness (t_s):

1.219

in

Lateral Design Factors - Table 12.3.1A (NDS)

D:	0.131	in	Diameter
F _{yb} :	100	ksi	Dowel Bending Yield Strength
F _{em} :	3,350	psi	Main Member dowel bearing strength
F _{es} :	3,350	psi	Side Member dowel bearing strength
l _m :	1.5	in	Main Member dowel bearing length
l _s :	1.219	in	Side Member dowel bearing length
R _d :	2.2		Reduction term - Table 12.3.1B (NDS)
R _e :	1		= F _{em} /F _{es}
R _t :	1.2		= l _m /l _s
k ₁ :	0.466		See Table
k ₂ :	1.111		See Table

Reference Lateral Design Values - Table 12.3.1A (NDS)

Z_I:

299

lbs

$Z_{Im} = \frac{Dl_mF_{em}}{R_d}$
(EQ 12.3 – 1)

Z_{II}:

113

lbs

$Z_{II} = \frac{k_1Dl_sF_{es}}{R_d}$
(EQ 12.3 – 3)

Z_{III}:

111

lbs

$Z_{III_m} = \frac{k_2Dl_mF_{em}}{(1 + 2R_e)R_d}$
(EQ 12.3 – 4)

Z_{IV}:

82

lbs

$Z_{IV} = \frac{D^2}{R_d} \sqrt{\frac{2F_{em}F_{yb}}{3(1 + R_e)}}$
(EQ 12.3 – 6)

Z_{MIN}:

82

lbs

Note: Side member is part of the Jeld-Wen assembly and verified during testing. Modes Z_{Is} and Z_{IIIs} are not applicable to the calculation.

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Subject: Wood Screw Lateral Design - Single Shear Cont.

Adjusted Lateral Design Values

$Z' = Z * C_D * C_M * C_t * C_g * C_{\Delta}$ – As per table 11.3.1 NDS

C _D :	1.6	Load Duration Factor - Table 2.3.2 (NDS)
C _M :	1.0	Wet Service Factor - Table 11.3.3 (NDS)
C _t :	1.0	Temperature Factor - Table 11.3.4 (NDS)
C _g :	1.0	Group Action Factor - Section 11.3.6 (NDS)
C _Δ :	1.0	Geometry Factor - Section 12.5.1.1 (NDS)

Z': 132 lbs

Fastener Bending Across Shim Space

Ω:	1.67	
L:	0.25	in Maximum Shim Gap
D:	0.131	in Diameter
F _{yb} :	100	ksi Dowel Bending Yield Strength

$\frac{F_{yb}}{\Omega} = \frac{M}{S} = \frac{16ZL}{\pi D^3} \Leftrightarrow Z = \frac{F_{yb}\pi D^3}{16\Omega L}$ Where $M = \frac{ZL}{2}$ (Guided Bending)

Z_n/Ω: 106 lbs

Bearing on Masonry Strap

Ω:	3.00	
F _u :	33	ksi Tensile Strength of strap
t:	20	GA
t:	0.036	in thickness of strap
D:	0.131	in

$\frac{P_{nv}}{\Omega} = 2.7 * t * D * F_u$ – (EQ.J4.3.1 – 4, AISI S100)

P_{nv}/Ω: 140 lbs

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Subject: Tapcon Lateral Design

Input:

Calculation:

Tapcon Size:

Size:	3/16	
D:	0.1875	in Nominal Diameter
D _{sh} :	0.145	in Shank Diameter

Fastener Shear Capacity - 3,000 psi Concrete

P_{nv}/Ω: 181 lbs See Table 1B of NOA 24-0102.06

Fastener Shear Capacity - Medium-Weight CMU

P_{nv}/Ω: 135 lbs See Table 3 of NOA 24-0102.06

Note:

- Critical anchor spacing is 16D
- Minimum Anchor Embedment is 1-1/4"
- Minimum Edge Distance is 2-1/4"

Fastener Bending Across Shim Space

L:	0.25	in Maximum Shim Gap
D _{sh} :	0.145	in Shank Diameter of Tapcon
F _{yb} :	100	ksi Yield Strength of Tapcon

Ω: 3.00

$$\frac{F_{yb}}{\Omega} = \frac{M}{S} = \frac{16P_n L}{\pi D^3} \Leftrightarrow P_n = \frac{F_{yb} \pi D^3}{16 \Omega L}$$

Where $M = \frac{P_n L}{2}$ (Guided Bending)

P_n/Ω: 239 lbs

Bearing Strength of Masonry Straps - AISI S100

Size:	3/16	Tapcon Size
D _{sh} :	0.145	in Shank Diameter of Tapcon Screw
F _u :	33	ksi Tensile Strength of Masonry Strap
t:	20	GA
t:	0.0359	in Thickness of Masonry Strap

Ω: 3.00

$$\frac{P_{nv}}{\Omega} = 2.7 * t * D * F_u - (EQ. J4.3.1 - 3, AISI S100)$$

P_{nv}/Ω: 155 lbs